

## Nondimensionalization - Logistic Model

$$(1) \quad \frac{dP}{d\pi} = rP \left(1 - \frac{P}{K}\right) \quad P(0) = P_0$$

where  $P$  is population (number  $N$ )  
at (dimensional) time  $\pi$

$$[P] = N \quad \text{number}$$

$$[\pi] = \pi \quad \text{time}$$

One can deduce from (1) that

$$[r] = \pi^{-1} \quad [K] = N \quad [P_0] = N$$

Introduce dimensionless dependent  
and independent variables

$$(2) \quad p = P/P^* \quad t = \pi/\pi^*$$

where  $P^*, \pi^*$  are to be determined  
and  $[P^*] = N, [\pi^*] = \pi$

Using (2) in (1) yields

$$\frac{dp}{dt} = (r\pi^*) p \left(1 - p \frac{P^*}{K}\right) \quad p(0) = P_0/P^*$$

Generally pick  $\pi^*, P^*$  s.t. resulting problem  
is as simple as possible.

$$(3) \quad \frac{dp}{dt} = p(1-p) \quad p(0) = \alpha$$

where  $\alpha = P_0/K$  using the choice

$$\pi^* = r^{-1} \quad P^* = K$$

## Advantages

- (1) Dimensionless model has fewer parameters
- (2) Sometimes small parameters exposed to aid in approximation schemes

## Note:

- (1) The choice of  $\pi^*$ ,  $P^*$  are not unique. For example, the choice

$$\pi^* = 2r^{-1} \quad P^* = P_0$$

would have resulted in

$$\frac{dp}{dt} = 2p(1 - \beta p) \quad p(0) = 1$$

where  $\beta = P_0/K$ .

In our case the solution is relatively simple

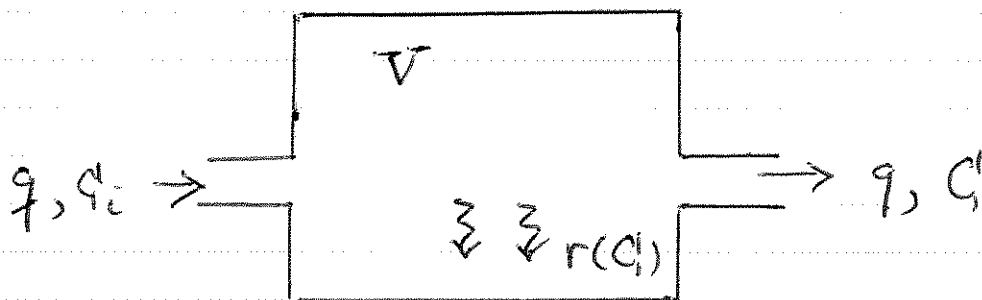
$$p(t) = \frac{\alpha}{\alpha + (1 - \alpha)e^{-t}}$$

## Continuously Stirred Tank Reactor (CSTR)

Chemical enters solvent filled tank of volume  $V$  at constant rate  $q$  with concentration  $C_i$ .

Tank contents are rapidly stirred so intratank concentration  $C$  is different than  $C_i$  in general.

Solvent reacts with reactant. Reactant disappears at rate  $r(C)$ .



Here

$$[V] = L^3$$

$$[C] = ML^{-3}$$

$$[q] = L^3 T^{-1} \quad \text{volume/time}$$

$$[r] = ML^{-3} T^{-1} \quad \text{mass/volume/time}$$

The latter defines what we mean by  $r$ .

Note: rate  $r$  is a function  $r(C)$  of  $C$

At any given (dimensional) time  $\tau$

$V C_1$  = total mass of reactant  
in tank.

Thus, conservation of mass implies

$$\frac{d}{d\tau}(V C_1) = \underset{\text{in}}{q C_{1i}} - \underset{\text{out}}{q C_1} - \underset{\text{reaction}}{V r(C_1)}$$

Depending on the reactant  $r(C_1)$  has  
different forms using Law of Mass  
Action

$$r(C_1) = k C_1 \qquad r(C_1) = \frac{k_1 C_1}{k_2 + C_1}$$

Using the former (as an assumption)

$$\begin{aligned} \frac{dC_1}{d\tau} &= \frac{q}{V} (C_{1i} - C_1) - k C_1 \\ C_1(0) &= C_{10} \quad (\text{initial tank}) \end{aligned}$$

is a model for  $C_1$  at time  $\tau$

Depends on many parameters

$$q \quad V \quad C_{1i} \quad k \quad C_{10}$$

## Non dimensionalization - CSTR model

$$(1) \quad \frac{dC}{d\tau} = \frac{q}{V} (C_i - C) - kC \quad C(0) = C_0$$

Introduce dimensionless variables

$$c = C/C_i^* \quad [C^*] = \text{ML}^{-3}$$

$$t = \tau/\tau^* \quad [\tau^*] = \tau$$

Yields

$$(2) \quad \frac{dc}{dt} = \frac{q\tau^*}{V} \left( \frac{C_i}{C_i^*} - c \right) - k\tau^*c \quad c(0) = \frac{C_0}{C_i^*}$$

There are many ways to choose  $C_i^*$  and  $\tau^*$ .

Two obvious choices for  $C_i^*$  are  $C_i^* = C_i, C_0$ .

CHOICE ONE  $C_i^* = C_i, \quad \frac{q\tau^*}{V} = 1$

$$(3) \quad \frac{dc}{dt} = (1-c) - \beta c \quad c(0) = \gamma$$

where

$$\beta = \frac{kV}{q} \quad \gamma = C_0/C_i$$

CHOICE TWO

$$C_1^* = C_1 \quad k\tau^* = 1$$

$$(4) \quad \frac{dc}{dt} = \frac{1}{\beta} (1-c) - c \quad c(0) = \gamma$$

where  $\beta, \gamma$  are as defined before.

Slow Reaction Rate  $\beta \ll 1$

$$\beta \ll 1$$

dimensionless

$$k \ll \frac{q}{V}$$

dimensional  
equivalent

Thus  $\beta \ll 1$  means the reaction rate  $k$  is small relative to the flow rate  $qV^{-1}$ .

$\beta \rightarrow 0^+$  approximation in CHOICE ONE

$$c(t) \cong 1 + (\gamma - 1)e^{-t} \quad \text{OK}$$

$\beta \rightarrow 0^+$  approximation in CHOICE TWO

$$c(t) \cong 1 \quad \text{X doesn't satisfy I.C.}$$

Thus CHOICE ONE appears to be advantageous wrt approximations

|| There is no a priori way to systematically choose a "best" nondimensionalization. ||

CHOICE THREE (Not in text!)

$$\frac{dc}{dt} = \frac{q\pi^*}{V} \left( \frac{C_i}{C^*} - c \right) - k\pi^* c$$

$$\frac{dc}{dt} = \left( \frac{q\pi^* C_i}{V C^*} \right) - \left( \frac{q\pi^*}{V} + k\pi^* \right) c$$

↑  
choose  $C^*$   
to make this  
one

↑  
choose  $\pi^*$  to make  
this one

Conclude (1-parameter model !!)

$$\boxed{\frac{dc}{dt} = 1 - c \quad c(0) = \alpha}$$

where

$$\pi^* = \left( k + \frac{q}{V} \right)^{-1}$$

$$C^* = \frac{C_i q}{q + kV}$$

and  $\alpha = C_0 / C^*$

Clearly this less obvious choice results in the simplest dimensionless model